Amendments to the Specification:

Please replace the section "Brief Description of the Drawings" with the following:

Figure 1 is a perspective view of the cassettes used to transport glass substrates;

Figure 2 is a diagrammatic depiction of the sag characteristics of conventional glass substrates within a cassette;

Figure 3 is a diagram of an embodiment of the invention showing the edges of the cured support members following an arc of a circle of predetermined radius.

Figures ~~3A~~ 4A and ~~3B~~ 4B are open and closed views, respectively, of the processing fixture in accordance with the present invention;

Figure [[4]] 5 is a diagram comparing the sag characteristics of each side of a glass substrate fabricated in accordance with the present invention relative to zero-gravity reference levels; and

Figure ~~5~~ 6 is a diagram comparing the sag characteristics of each side of glass substrate fabricated in accordance with the present invention.

Replace the first paragraph on page 4 under Detailed Description, beginning at line 21, with the following:

Reference will now be made in detail to the present exemplary embodiments of the invention, examples of which are illustrated in the accompanying drawings. Wherever possible, the same reference numbers will be used throughout the drawings to refer to the same or like parts. An exemplary embodiment of the processing fixture of the present invention is shown in Figure ~~3A~~ 4A and ~~3B~~ 4B, and is designated generally throughout by reference numeral 10.

Replace the two paragraphs beginning on page 5, line 7 and ending on page 5, line 29 with the following:

As embodied herein, and depicted in Figure ~~3A~~ 4A, a view of the open processing fixture 10 in accordance with the present invention is disclosed. Fixture 10 includes convex end cap 12 which contacts curved support member 14 by adjustable alignment pins 16. Subsequent support members 14 also contact adjacent support members 14 by alignment pins 16. Finally, the last support member 14 contacts concave end cap 18. Figure ~~3A~~ 4A shows fixture 10 in an open configuration that is suitable for loading the glass substrates. Initially, the first substrate to be loaded is placed on the curved surface of end cap 18. Subsequently, a support member 14 is placed over the glass substrate. This process continues until convex end cap 12 is placed over the last substrate to be loaded into fixture 10. After loading, fixture 10 is rotated 90°.

Figure ~~3B~~ 4B is a closed view of fixture 10 as disposed in a suitable furnace. In practice, a temperature range between 400° C and 700° C is used. Depending on the temperature, the glass is heated for a time period of up to two hours. The heating causes a molecular structural rearrangement of the glass and the glass conforms to the shape of curved support members 14. While in fixture 10, the substrates are not firmly held or molded by the curved supports 14. Nonetheless a preferential shape is imparted, and a slight bow is formed in the substrate. With the aforementioned thermal conditioning, the imparted shape may be retained. The processed substrates have greater shape consistency and improved sag characteristics. The benefit of remaining loosely held, yet constrained, is that the desired shape can be created while allowing for thermal expansions and contractions to occur without glass breakage. A further benefit comes from the bowed shape during processing, whereby the substrates are somewhat self-supporting and less susceptible to gravity effects.

Replace the two paragraphs beginning on page 6, line 28 and ending on page 7, line 28 with the following:

Referring to Figure [[4]] 5, a diagram comparing the sag characteristics of each side of a glass substrate fabricated in accordance with the present invention relative to zero-gravity reference levels is disclosed. Referring to Side 1, S_{01} refers to the shape of the glass substrate when the concave side of the bowed substrate is oriented upward

under zero gravity conditions. S_1 refers to the shape of the glass substrate when the concave side of the bowed substrate is oriented upward under normal conditions typically encountered on earth. Δ_1 refers to the maximum sag from the zero gravity position. Referring to Side 2, S_{02} refers to the shape of the glass substrate when the concave side of the bowed substrate is oriented downward under zero gravity conditions. S_2 refers to the shape of the glass substrate when the concave side of the bowed substrate is oriented upward under normal conditions typically encountered on earth. Δ_2 refers to the maximum sag from the zero gravity position. Comparing side 1 to side 2, it is seen that $\Delta_1 \approx \Delta_2$, that is, the distance between the zero gravity position and the final resting position of the sagged substrate is essentially equivalent, regardless of which side is facing upward. Referring to Side 2, it is noted that the maximum deformation of the concave bow is the maximum distance between line S_{02} and the horizontal reference. This distance is typically on the order of approximately 1mm. Changing the reference to the zero sag plane (horizontal reference) gives us the case from which sag values are derived.

Figure ~~5~~ 6 compares the sag characteristics as measured from the zero sag plane (horizontal reference) for each side of a glass substrate fabricated in accordance with the present invention. Figure ~~5~~ 6 is a diagram that is very similar to Figure [[4]] 5. Again, S_1 refers to the shape of the glass substrate when the concave side of the bowed substrate is oriented upward under normal conditions, whereas S_2 refers to the shape of the glass substrate when the concave side of the bowed substrate is oriented upward. However, in this diagram Δ_1 refers to the maximum sag of side 1 from the horizontal and Δ_2 refers to the maximum sag of side 2 from the horizontal. As expected, $\Delta_1 > \Delta_2$. Thus, for a bowed substrate, the amount of sag will be reduced when the concave side of the substrate is oriented downward. The concave side down orientation is the preferred orientation in a cassette. Thus, the benefits of the present invention are manifest. The induced shape change directly decreases the sag maxima. By imparting the shape change to the substrate, the substrate is provided a consistent shape that results in decreased sag variability from substrate to substrate.